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# HIGH EFFICIENCY SEMI-FUEL CELL INCORPORATING AN ION EXCHANGE MEMBRANE

#### TO ALL WHOM IT MAY CONCERN

BE IT KNOWN THAT (1) MARIA G. MEDEIROS, (2) ERIC G. DOW, employees of the United States Government, (3) RUSSELL R. BESSETTE, (4) SUSAN G. YAN, AND (5) DWAYNE W. DISCHERT, citizens of the United States of America, and residents of (1) Bristol, County of Bristol, State of Rhode Island, (2) Barrington, County of Bristol, State of Rhode Island, (3) Mattapoisett, County of Plymouth, Commonwealth of Massachusetts, (4) Fairport, County of Monroe, State of New York, and (5) Middletown, County of Newport, State of Rhode Island, have invented certain new and useful improvements entitled as set forth above of which the following is a specification:

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FAX:

1	Attorney Docket No. 82737
2	
3	HIGH EFFICIENCY SEMI-FUEL CELL
4	INCORPORATING AN ION EXCHANGE MEMBRANE
5	
6	STATEMENT OF GOVERNMENT INTEREST
7	The invention described herein may be manufactured and used
8	by or for the Government of the United States of America for
9	governmental purposes without the payment of any royalties
10	thereon or therefore.
11	
12	CROSS REFERENCE TO OTHER RELATED APPLICATIONS
13	This patent application is co-pending with a related patent
14	application entitled METHOD TO ACCELERATE WETTING OF AN ION
15	EXCHANGE MEMBRANE IN A SEMI-FUEL CELL (Navy Case No. 84277), by
16	Louis G. Carreiro, Charles J. Patrissi, and Steven P. Tucker,
17	employees of the United States Government, and related patent
18	application entitled A BIPOLAR ELECTRODE FOR USE IN A SEMI-FUEL
19	CELL (Navy Case No. 84257) by Charles J. Patrissi, Maria G.
20	Medeiros, Louis G. Carreiro, Steven P. Tucker, Delmas W.
21	Atwater, employees of the United States Government, Russell R.
22	Bessette and Craig M. Deschenes.

#### BACKGROUND OF THE INVENTION

- 2 (1) Field of the Invention
- 3 The present invention relates to electrochemical systems
- 4 and more specifically to a novel semi-fuel cell design based on
- 5 a seawater electrolyte and liquid catholyte combination that
- 6 uses an ion exchange membrane to isolate the seawater
- 7 electrolyte and liquid catholyte combination from the seawater
- 8 anolyte solution.
- 9 (2) Description of the Prior Art
- 10 Primary batteries employing aqueous electrolytes have been
- 11 under investigation for several years leading to the development
- 12 of semi-fuel cells, a hybrid of fuel cells and batteries that
- 13 combine the refillable cathode or catholyte oxidizer of fuel
- 14 cells with the consumable anode fuel of batteries. The metal
- 15 anode and liquid catholyte are consumed to produce energy.
- 16 Semi-fuel cells are currently being considered as
- 17 electrochemical energy sources for unmanned undersea vehicles
- due to the availability of seawater to act as an electrolyte in
- 19 combination with the liquid catholyte or alone as the anolyte
- 20 solution. The semi-fuel cell anode is often made of aluminum,
- 21 magnesium or lithium due to the high faradaic capacity, low
- 22 atomic weight and high standard potential of these metals. The
- 23 catholyte is usually a strong oxidizer such as hydrogen peroxide
- 24 in solution with the seawater electrolyte.

- Seawater semi-fuel cells, also known as solution phase
- 2 semi-fuel cells because the catholyte is in solution with the
- 3 seawater, are an ideal electrochemical energy source for
- 4 undersea vehicles. The use of seawater from the undersea
- 5 vehicle's surroundings minimizes the volume and weight of
- 6 reactants that need to be carried in the vehicles. This
- 7 provides an important weight savings to the vehicle. Seawater
- 8 semi-fuel cells have a high faradaic capacity, and have a high
- 9 energy density at low current densities while being relatively
- 10 inexpensive, environmentally friendly, capable of a long shelf
- 11 life, and not prone to spontaneous chemical or electrochemical
- 12 discharge.
- In order to meet the high energy density requirements of
- 14 underwater vehicles semi-fuel cells currently being developed
- 15 are used in stack or multi-stack configurations. The use of
- 16 bipolar electrodes having an anode on one side and a catalyzed
- 17 cathode on the other is beneficial in minimizing cell stack size
- 18 and weight.
- In prior art semi-fuel cells, each cell is hydraulically
- 20 fed in parallel with a seawater and/or sodium hydroxide (NaOH)
- 21 aqueous electrolyte. The catholyte is carried separately and
- 22 injected directly into the seawater and/or seawater/sodium
- 23 hydroxide mixture upstream of the stack inlet at the required
- 24 concentration, determined by the system power load.

- Electrochemical reduction of the catholyte, occurs on the
- electrocatalyst surface of the cathode current collector, 2
- receiving electrons from the anode oxidation reaction. 3
- The electrochemical reactions for an aluminum hydrogen
- 5 peroxide semi-fuel cell are given below:

$$HO_2^- + H_2O + 2e^- -> 3OH^-$$
  $E^0 = 0.88 \text{ V}$ 

$$E^{o} = 0.88 \text{ V}$$

$$Al + 4OH^{-} -> AlO_{2}^{-} + 2H_{2}O + 3e^{-}$$
  $E^{o} = -2.33 \text{ V}$ 

$$E^{\circ} = -2.33 \text{ V}$$

8 Cell Reaction: 
$$2Al + 3 HO_2^- -> 2AlO_2^- + OH^- + H_2O$$
  $E_{cell} = 3.21 V$ 

$$E_{cell} = 3.21 \text{ V}$$

- In addition to the primary electrochemical reaction, the 9
- following undesired parasitic reactions can also take place: 10

$$2A1 + 2H_2O + 2OH^- -> 2AlO_2^- + 3H2$$

Direct Reaction: 
$$2A1 + 3H_2O_2 + 2OH^- \rightarrow 2A1O_2 + 4H_2O$$

$$2H_2O_2 -> 2H_2O + O_2 \uparrow$$

- The electrochemical reactions for a magnesium hydrogen 14
- peroxide semi-fuel cell are given below: 15

$$Mg -> Mg^{2+} + 2e^{-}$$

$$E^{o} = -2.37 v$$

$$H_2O_2 + 2H^+ + 2e^- \rightarrow 2 H_2O$$
  $E^0 = 1.77 v$ 

$$E^{\circ} = 1.77 \text{ v}$$

$$Mg + H_2O_2 + 2H^+ -> Mg^{2+} + 2 H_2O E_{cell} = 4.14v$$

$$E_{cell} = 4.14v$$

- In addition to the primary electrochemical reaction, the 19
- following undesired parasitic reactions could also take place: 20
- Decomposition: 21

$$2 H_2O_2 \rightarrow 2H_2O + O_{2(\alpha)}$$

$$Mg + H_2O_2 + 2H^+ -> Mg^{2+} + 2H_2O$$

$$Mg + 2H_2O -> Mg^{2+} + 2 OH^- + H_{2(g)}$$

The electrochemical reactions for the lithium -hydrogen

2 peroxide semi-fuel cell are given below:

3 Anode: 
$$\text{Li} -> \text{Li}^{+} + \text{e}^{-}$$
  $\text{E}^{\circ} = -3.04 \text{ v}$ 

4 Cathode: 
$$H_2O_2 + 2H^+ + 2e^- \rightarrow 2 H_2O$$
  $E^0 = 1.77 v$ 

5 Cell Reaction: 
$$2Li + H_2O_2 + 2H^+ -> 2Li^+ + 2 H_2O$$
  $E_{cell} = 4.81v$ 

In addition to the primary electrochemical reactions, the

7 following undesired parasitic reactions could also take place:

8 Decomposition: 
$$2 H_2O_2 \rightarrow 2H_2O + O_2$$

9 Direct Reaction: Li + 
$$H_2O_2$$
 +  $2H^+$  ->  $2Li^+$  + 2  $H_2O_3$ 

10 Corrosion: 
$$2Li + 2H_2O -> 2Li^+ + 2OH^- + H_{2(q)}$$

Of the parasitic reactions listed above, the direct

12 reactions are the most detrimental to the operation of the semi-

13 fuel cell since both the metal anode, either magnesium, aluminum

14 or lithium and the the hydrogen peroxide cathologte are consumed

in a single step. A direct reaction occurs when the catholyte,

in this case  $H_2O_2$ , is allowed to come into direct physical

17 contact with the metal anode, resulting in a chemical reaction

18 which does not produce electron transfer and only consumes

19 active energetic materials, thus reducing the overall energy

20 yield of the semi-fuel cell. In most cases this parasitic

21 reaction will consume over 50% of the available energetic

22 materials.

Whereas magnesium, lithium or aluminum corrosion can be

24 suppressed by pH adjustment and hydrogen peroxide decomposition

- 1 minimized by careful temperature control, in order to minimize
- 2 or completely prevent the parasitic direct reaction, the metal
- 3 anode side of the bipolar electrode must be physically isolated
- 4 from the liquid catholyte.
- 5 What is needed is a semi-fuel cell that enables the
- 6 separation of the metal anode from the catholyte while
- 7 maintaining necessary ion transfer to affect the necessary
- 8 electrochemical balance for the reaction to take place. This is
- 9 accomplished through a new semi-fuel cell design that
- 10 incorporates an ion exchange membrane to allow a separated flow
- of anolyte and catholyte in the semi-fuel cell thereby isolating
- 12 the metal anode of the bipolar electrode from the catholyte.

13

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#### SUMMARY OF THE INVENTION

- It is a general purpose and object of the present invention
- 16 to eliminate the parasitic direct reaction of the catholyte with
- 17 the metal anode in a semi-fuel cell, thereby improving the
- 18 overall energy yield of the semi-fuel cell.
- 19 This general purpose and object is accomplished with the
- 20 present invention by using a semi-permeable membrane capable of
- 21 ion exchange placed between the anode and cathode compartment of
- 22 a semi-fuel cell in order to isolate the anolyte and catholyte
- 23 solutions.

## BRIEF DESCRIPTION OF THE DRAWINGS

2	FIG.	1	shows	part	of	a	semi-fue	l cell	stack	with	a	membrane
				_						•		
3	separatin	a 1	the and	olvte	fro	m	the cath	olyte.				

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### DESCRIPTION OF THE PREFERRED EMBODIMENT

Referring now to FIG. 1 there is shown part of semi-fuel
cell stack 10 with a metal anode 12 and a catalyzed cathode 14.
In a preferred embodiment, the metal anode is aluminum or

9 magnesium, however, it can also be lithium or other suitable

11 12 and cathode 14 is a flow path 30 through which two separate

metals or alloys and is not limited as such. Between the anode

12 electrolyte fluids the anolyte 16 and catholyte 18 may flow from

their respective reservoirs 32 and 34. In a preferred

14 embodiment, the analyte 16 is seawater or aqueous sodium

15 hydroxide, and the catholyte 18 is hydrogen peroxide in solution

16 with seawater or aqueous sodium hydroxide and/or acid.

17 Separating the flow path 30 into two separate compartments is an

18 ion exchange membrane 20 that is electrically conductive,

19 capable of exchanging ions and is resistant to both the anolyte

20 16 and the catholyte 18. When the metal anode 12 is magnesium

21 or lithium, a cation exchange membrane is favored. When the

22 metal anode 12 is aluminum, an anion exchange membrane is

23 favored. In the preferred embodiment, the membrane 20 is a

24 perfluorinated ionomer membrane such as Nafion®, however other

- 1 ion exchange membranes such as Flemion®, Aciplex XR®, Gore®, PBI
- 2 (polybenzimidayole), PES (poly-p-phenylene ether sulfone), PEEK
- 3 (poly-p-phenylether ether ketone) can be used. The membrane 20
- 4 can also be a microporous membrane such as Viskase®, Celgard®,
- 5 FAS® or UCB® Films. The membrane 20 is situated such that the
- anolyte 16 flows on one side of the membrane 20 making contact
- 7 only with the metal anode 12. On the other side of the membrane
- 8 the catholyte 18 flows into the flow path 30 making contact only
- 9 with the catalyzed cathode 14. In this way the anode 12 is
- 10 physically separated from the cathloyte 18 by the membrane 20
- 11 that separates the two electrolytes but allows ions to pass
- 12 through it maintaining the necessary ion transfer to affect the
- 13 proper electrochemical balance for the reaction to take place.
- 14 The advantages of the present invention over the prior art
- 15 are that the electrochemical efficiency of a semi-fuel cell is
- 16 improved by nearly 80% by virtue of reducing and even
- 17 eliminating the parasitic direct reaction. Furthermore with the
- 18 separate flow of the anolyte 16 and catholyte 18, corrosion of
- 19 the metal anode 12 can now be suppressed by separately adjusting
- 20 the pH of the anolyte 16 and catholyte 18 in their individual
- 21 respective reservoirs 32 and 34. In addition the decomposition
- 22 parasitic reaction is also reduced because the catholyte 18 is
- 23 not heated. Under normal operating conditions the analyte 16
- 24 may be heated to facilitate the electrochemical reaction. This

- 1 is especially true when the metal anode 12 is aluminum. In
- 2 prior art semi-fuel cells electrolytes contained both the
- 3 anolyte 16 and catholyte 18 in the same solution. However,
- 4 heating the hydrogen peroxide catholyte 18 accelerates the
- 5 decomposition parasitic reaction generating oxygen gas, which is
- 6 an undesirable byproduct, particularly in underwater vehicles.
- 7 By separating the flow of the anolyte 16 and catholyte 18
- 8 through the use of the ion exchange membrane 20, the analyte 16
- 9 can be heated in its own reservoir 32 by a heater 36 without
- 10 heating the catholyte 18.
- Other advantages of the present invention include a reduction in
- 12 the amount of reactants that need to be carried in the undersea
- 13 vehicle employing the semi-fuel cell. The high efficiencies minimize
- 14 the necessary reactants thus lowering the overall weight and volume
- of the undersea vehicle. The high efficiencies also lower the gas
- 16 generation due to corrosion, decomposition or other inefficiencies.
- 17 Lower corrosion rates of the anode also translate to prolonged anode
- 18 lifetime.
- 19 Obviously many modifications and variations of the present
- 20 invention may become apparent in light of the above teachings. For
- 21 example, the metal anode may be made of a variety of metals or
- 22 alloys. Instead of an ion exchange membrane a micro-porous membrane
- 23 could be used.

- In light of the above, it is therefore understood that
- 2 within the scope of the appended claims, the invention may be
- 3 practiced otherwise than as specifically described.

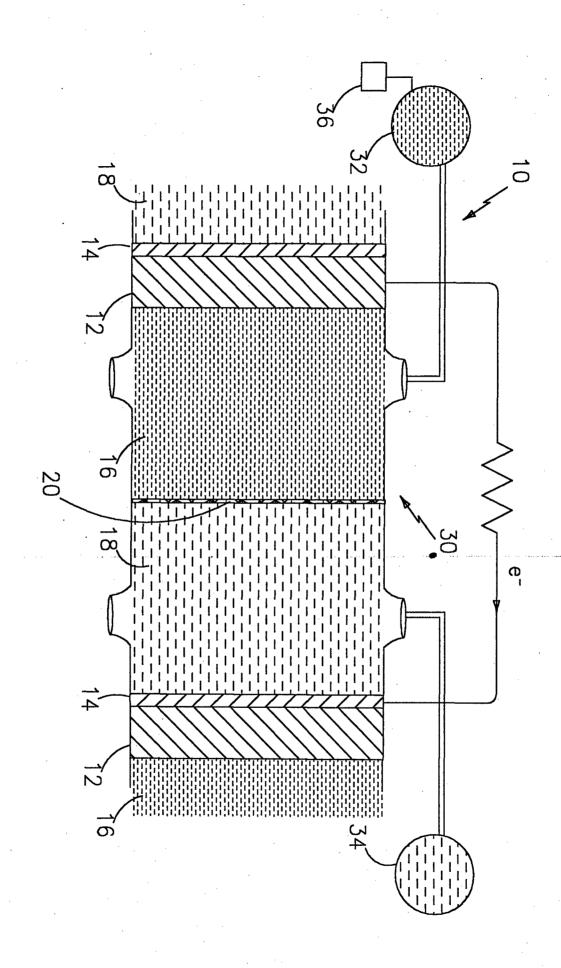


FIG. 1